



## (Gd, Co, Ta)-Doped SnO<sub>2</sub> Varistor Ceramics

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**Abstract.** The effect on the microstructure and electrical properties of (Co, Ta)-doped SnO<sub>2</sub> varistors upon the addition of Gd<sub>2</sub>O<sub>3</sub> was investigated. The threshold electric field of the SnO<sub>2</sub> based varistors increased significantly from 720 V/mm to 1455 V/mm, the relative dielectric constants of the SnO<sub>2</sub> based varistors decreased greatly from 833 to 330 as Gd<sub>2</sub>O<sub>3</sub> concentration was increased up to 1.2 mol%. The significant decrease of the SnO<sub>2</sub> mean grain size, from 3.8 to 1.6 μm with increasing Gd<sub>2</sub>O<sub>3</sub> concentration over the range of 0 to 1.2 mol%, is the origin for increase in the threshold voltage and decrease of the dielectric constants. The mean grain size reduction is attributed to the segregation of Gd<sub>2</sub>O<sub>3</sub> at grain boundaries hindering the SnO<sub>2</sub> grains from conglomerating into large particles. Varistors were found to have superhigh threshold voltage and comparatively large nonlinear coefficient  $\alpha$ . For 0.8 mol% Gd<sub>2</sub>O<sub>3</sub>-doped sample, threshold electrical field  $E$  and nonlinear coefficient  $\alpha$  were measured to be 1125 V/mm and 24.0, for 1.2 mol% Gd<sub>2</sub>O<sub>3</sub>-doped sample,  $E$  and  $\alpha$  were 1355 V/mm and 23.0. Superhigh threshold voltage and large nonlinear coefficient qualify the Gd-doped SnO<sub>2</sub> varistor as an excellent candidate in use for high voltage protection system.

**Keywords:** SnO<sub>2</sub>, varistor, electrical nonlinearity, grain boundary barrier

### Introduction

Varistor materials with high nonlinearity in their current-voltage characteristics are used as protecting devices against voltage transients in electronic and industrial equipment and as surge arrestors. The combination of high nonlinearity and high-energy absorption capability coupled with low power loss has made the ZnO varistor extremely attractive for high power applications [1–4]. However, with the increasing use of this device as the surge-suppressing element, the requirement of long-range-stability varistor is becoming more important.

In recent years, some papers have been published on novel SnO<sub>2</sub>-based varistors. Pianaro et al. succeeded in preparing SnO<sub>2</sub>-based varistor ceramics by doping with Co<sub>2</sub>O<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub>, they found that SnO<sub>2</sub>-based ceramics doped with 1.00 mol% CoO and 0.05

mol% Nb<sub>2</sub>O<sub>5</sub> were a promising varistor material [5–9]. Wang et al. found that (Zn, Nb) doped SnO<sub>2</sub> and (Co, Sb) doped SnO<sub>2</sub> also exhibit varistor nonlinearity [10, 11].

In this paper, the effect of Gd<sub>2</sub>O<sub>3</sub> addition on the properties of (Co, Ta)-doped SnO<sub>2</sub> varistors was investigated. It was found that Gd<sub>2</sub>O<sub>3</sub> addition not only greatly raised the threshold voltage of the (Co, Ta)-doped SnO<sub>2</sub> varistors, but also significantly reduced the dielectric constant of the (Co, Ta)-doped SnO<sub>2</sub> varistors. The mean grain size reduction was attributed to the segregation of Gd<sub>2</sub>O<sub>3</sub> at grain boundaries which hinder the SnO<sub>2</sub> grains from conglomerating into large particles.

### Experimental Procedure

The composition used in mol% was: (99.15 –  $x$ )% SnO<sub>2</sub> + 0.75% Co<sub>2</sub>O<sub>3</sub> + 0.1% Ta<sub>2</sub>O<sub>5</sub> +  $x$ % Gd<sub>2</sub>O<sub>3</sub>, with  $x$ : 0.0, 0.4, 0.8 and 1.2. The reagents used in

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Table 1. Characteristics of (Gd, Co, Ta)-doped SnO<sub>2</sub> varistors.

Gd <sub>2</sub> O <sub>3</sub> (mol%)	Mean grain size (μm)	α	Density (g/cm <sup>3</sup> )	Relative density (%)	E <sub>1mA</sub> (V/mm)	φ <sub>B</sub> (eV)	ε <sub>r</sub> (1 kHz)	R <sub>gb</sub> (Ω · cm)	R <sub>gr</sub> (Ω · cm)
0.00	3.8	14	6.80	97.8	610	1.14	833	52.9 × 10 <sup>6</sup>	1.50 × 10 <sup>3</sup>
0.4	2.6	23	6.78	97.5	935	1.13	545	24.5 × 10 <sup>6</sup>	1.95 × 10 <sup>3</sup>
0.8	2.0	24	6.76	97.2	1125	1.07	406	–	–
1.2	1.6	23	6.71	96.5	1355	1.02	330	21.2 × 10 <sup>6</sup>	2.35 × 10 <sup>3</sup>

Theoretical density of SnO<sub>2</sub> is 6.95 g/cm<sup>3</sup>.

this study were analytical-grade SnO<sub>2</sub> (99.5%), Co<sub>2</sub>O<sub>3</sub> (99.5%), Ta<sub>2</sub>O<sub>5</sub> (99.95%) and Gd<sub>2</sub>O<sub>3</sub> (99.95%). The chemicals were wet-milled in polyethylene bottles with ZrO<sub>2</sub> balls for 12 h in deionized water. The milled powders were dried, ground and granulated with PVA binder. The granulated powder were pressed into discs 15 mm in diameter by 1.0 mm in thickness at a pressure of 150 MPa. After burning out the PVA at 650°C, the discs were put into Al<sub>2</sub>O<sub>3</sub> crucibles and fully surrounded with the powder of matching compositions, sintered in air at 1300°C for 1 hour and then cooled to room temperature freely. Silver paste was applied on the faces of the sintered discs to form electrodes by firing at 550°C. The sample phase was observed by X-ray diffraction (XRD) using CuKα radiation. For microstructure characterization, the samples were analyzed by scanning electron microscopy (SEM). For electrical characterization of current density versus applied electrical field, an I-V plotter (QT2) was used. The permittivity and the impedance were determined with impedance analyzer (Agilent 4294A) in the frequency range of 40 Hz–15 MHz. The electrical nonlinear coefficient α was obtained by

$$\alpha = \frac{\log(I_2/I_1)}{\log(V_2/V_1)}, \quad (1)$$

where V<sub>1</sub> and V<sub>2</sub> are, respectively, the voltage at current I<sub>1</sub> and I<sub>2</sub>. For a Schottky type of mechanism, the current density of a varistor is related to the electric field and temperature by the equation [6]

$$J = AT^2 \exp[(\beta E^{1/2} - \phi_B)/kT], \quad (2)$$

where A is Richardson's constant, k is Boltzmann constant, φ<sub>B</sub> is the interface barrier height, and β is a constant related to the grain size and the barrier width. In order to reduce the rise in temperature of the specimen caused by the electric current, we made the current

flowing through the specimen in μA range and put the specimen in silicon oil. By use of equations

$$J_1 = AT^2 \exp[(\beta E_1^{1/2} - \phi_B)/kT], \quad (3)$$

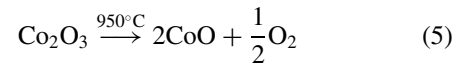
$$J_2 = AT^2 \exp[(\beta E_2^{1/2} - \phi_B)/kT], \quad (4)$$

one can calculate φ<sub>B</sub>. The data of the varistor system are listed in Table 1.

## Results and Discussion

Figure 1 shows the X-ray diffraction pattern, (a) for the pure SnO<sub>2</sub> powder and (b) for SnO<sub>2</sub> varistor doped with 1.2 mol% Gd<sub>2</sub>O<sub>3</sub>. It was observed from the X-ray diffraction pattern that there was no apparent second any phases besides SnO<sub>2</sub> phase. Second any phases produced by dopants were too sparse to be detected by normal X-ray diffraction. The SEM micrographs of the as-fired surfaces of the varistors are shown in Fig. 2. It can be seen that the mean grain size of the SnO<sub>2</sub> based varistors decreases significantly, from 3.8 to 1.6 μm, with increasing Gd<sub>2</sub>O<sub>3</sub> concentration. All varistors have densities as high as 96.5% or more of that of SnO<sub>2</sub> crystal. The electrical nonlinear characteristic of the varistor system is shown in Fig. 3. It was observed that the threshold voltage of the SnO<sub>2</sub>-based varistors increased significantly from 720 V/mm to 1455 V/mm with increasing Gd<sub>2</sub>O<sub>3</sub> concentration over the range of 0 to 1.2 mol%.

The thermogravimetric analysis suggests that the dopants of Co<sub>2</sub>O<sub>3</sub> will be reduced to CoO with liberation of oxygen by the reaction [12]



Considering that the ionic radius of Co<sup>2+</sup> (0.078 nm) is close to that of Sn<sup>4+</sup> (0.071 nm), the introduction of

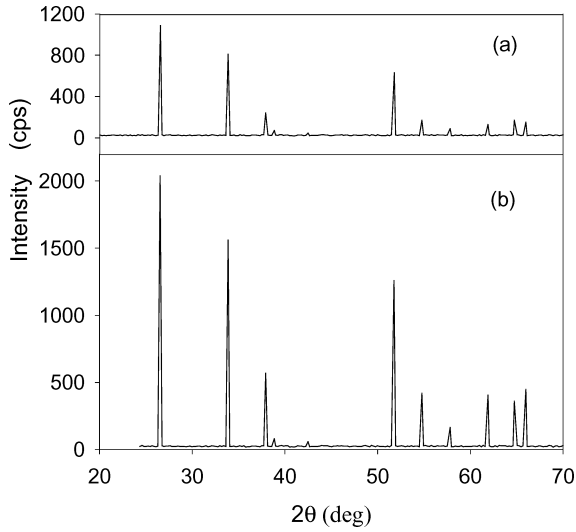


Fig. 1. X-ray diffraction, (a) pure SnO<sub>2</sub>, (b) (Co, Ta)-doped SnO<sub>2</sub> varistor with 2.5 mol% Gd<sub>2</sub>O<sub>3</sub>.

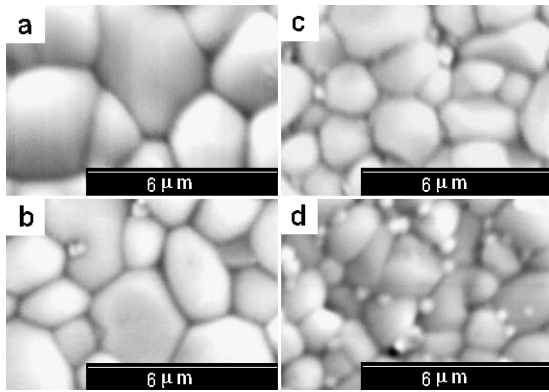
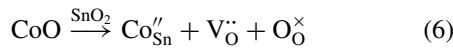


Fig. 2. SEM microstructure for (99.15 - x)%SnO<sub>2</sub> + 0.75%Co<sub>2</sub>O<sub>3</sub> + 0.1%Ta<sub>2</sub>O<sub>5</sub> + x% Gd<sub>2</sub>O<sub>3</sub> varistors (a) x = 0.0, (b) x = 1.5, (c) x = 2.0, (d) x = 2.5.

CoO to the SnO<sub>2</sub> lattice should lead to the reaction



where the Kröger-Vink marks [13] were used. Due to a small difference between the ionic radius of Ta<sup>5+</sup> (0.073 nm) and that of Sn<sup>4+</sup>, the substitution of Sn<sup>4+</sup> by Ta<sup>5+</sup> is the most likely to occur. The reaction can be written as

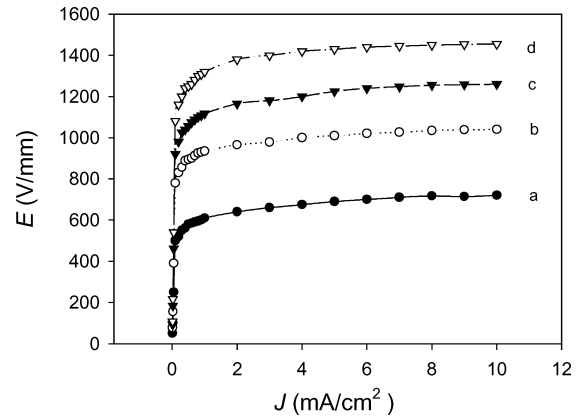
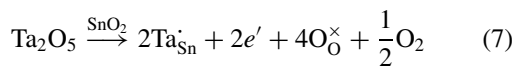
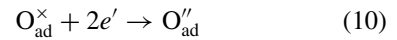
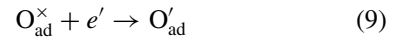


Fig. 3. Electric field versus current for (99.15 - x)%SnO<sub>2</sub> + 0.75%Co<sub>2</sub>O<sub>3</sub> + 0.1%Ta<sub>2</sub>O<sub>5</sub> + x% Gd<sub>2</sub>O<sub>3</sub> varistors, (a) x = 0.0, (b) x = 1.5, (c) x = 2.0, (d) x = 2.5.

Oxygen in the above equations will be partly absorbed at SnO<sub>2</sub> grain boundaries



Those absorbed oxygen easily capture electrons to become negatively charged ions



The role of the absorbed oxygen in the formation of boundary barriers was addressed in the literature [9, 14–16].

Because the ionic radius of Gd<sup>3+</sup> (0.094 nm) are larger than that of Sn<sup>4+</sup> (0.071 nm), the substitution of Sn<sup>4+</sup> by Gd<sup>3+</sup>, according to the reaction



will cause SnO<sub>2</sub> lattice to distort. That is, the reaction of Eq. (11) is less likely to proceed than the reactions of Eqs. (6) and (7) because the the reaction of Eq. (11) causing lattice distortion should be more energetic than the reactions of Eqs. (6) and (7). Due to the partial substitution of Sn<sup>4+</sup> by Gd<sup>3+</sup>, much more Gd<sub>2</sub>O<sub>3</sub> will have to reside at SnO<sub>2</sub> grain boundaries. Gd<sub>2</sub>O<sub>3</sub> residing at SnO<sub>2</sub> grain boundaries may hinders the SnO<sub>2</sub> grains, on both sides of the boundary, from conglomerating

into large particles. That may be the reason why the mean grain size of the SnO<sub>2</sub> based varistors decreased significantly with increasing Gd<sub>2</sub>O<sub>3</sub> concentration.

The threshold voltage,  $V_s$ , for a varistor is determined by the mean number of barriers  $\bar{N}$  in series multiplied by  $v_b$

$$V_s = \bar{N} \cdot v_b \quad (12)$$

where  $v_b$  is the barrier voltage at the grain boundary. From Table 1 we can see that the barrier height is roughly the same for the (Co, Ta, Gd)-doped SnO<sub>2</sub> varistors, therefore the threshold voltage,  $V_s$ , is roughly proportional to the mean number of barriers  $\bar{N}$ . If the thickness of a varistor is  $D$  and the mean grain size is  $d$ , it is clear from the relation  $D = \bar{N}d$  that  $\bar{N}$  is inversely proportional to mean grain size  $d$ . Thus, It is easily understood that the threshold voltage of the varistors increases significantly with increasing Gd<sub>2</sub>O<sub>3</sub> concentration due to the significant reduction of the mean grain size with increasing Gd<sub>2</sub>O<sub>3</sub> concentration.

The relative dielectric permittivity versus frequency for the varistor system is shown in Fig. 4. It is very clear that the dielectric constant of the varistor system decreases greatly with increasing Gd<sub>2</sub>O<sub>3</sub> concentration. The relative dielectric constants can be expressed as the following relation [3]

$$\varepsilon_r = \varepsilon_B d / t_B \quad (13)$$

where  $\varepsilon_B$  is the internal permittivity of the barrier material,  $d$  is the mean grain size and  $t_B$  is the mean thick-

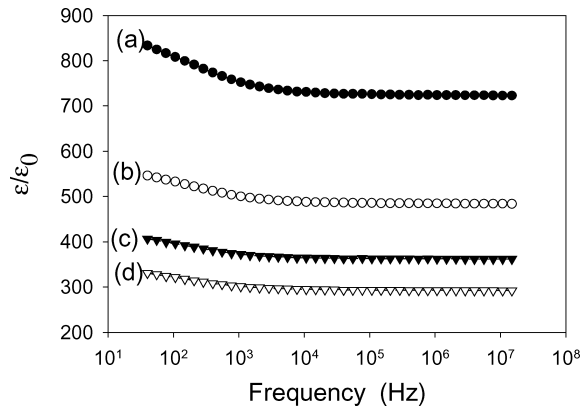


Fig. 4. Dielectric permittivity versus frequency for (99.15 -  $x$ )%SnO<sub>2</sub> + 0.75%Co<sub>2</sub>O<sub>3</sub> + 0.1%Ta<sub>2</sub>O<sub>5</sub> +  $x$ % Gd<sub>2</sub>O<sub>3</sub>, (a)  $x = 0.0$ , (b)  $x = 1.5$ , (c)  $x = 2.0$ , (d)  $x = 2.5$ .

ness of the insulation barrier. According to the Eq. (13), the permittivity of a varistor is proportional to the ratio  $d/t_B$ . From the fact in Table 1 that the barrier height is roughly the same for all Gd<sub>2</sub>O<sub>3</sub>-doped varistors one can deduce that the variation of  $t_B$  for all Gd<sub>2</sub>O<sub>3</sub>-doped varistors is small too. Therefore, the permittivity of the Gd<sub>2</sub>O<sub>3</sub>-doped varistors is mainly determined by the mean grain size  $d$ . So, the decrease of the permittivity of Gd<sub>2</sub>O<sub>3</sub>-doped varistors with increasing Gd<sub>2</sub>O<sub>3</sub> concentration is reasonable because the SnO<sub>2</sub> mean grain size decreases significantly with increasing Gd<sub>2</sub>O<sub>3</sub> concentration.

The impedance diagrams of  $-Z''$  (negative reactance) vs  $Z'$  (resistance) of a varistor usually takes a form of a semicircle. But the impedance diagrams of  $-Z''$  vs  $Z'$  of the Gd<sub>2</sub>O<sub>3</sub>-doped varistors measured at room temperature present a partial semicircle, which leads to a difficulty in distinguishing the contributions of boundaries from those of grains. To show a whole semicircle of the impedance diagrams of  $-Z''$  vs  $Z'$  of the Gd<sub>2</sub>O<sub>3</sub>-doped varistors, high-temperature measurements at 250°C were performed. The impedance diagrams of  $-Z''$  vs  $Z'$  of the Gd<sub>2</sub>O<sub>3</sub>-doped varistors are shown in Fig. 5. The resistivities of grains are determined to be approximately 1.50, 1.95, 2.35 kΩ · cm at the frequency of 13 MHz for samples doped with 0.0, 0.4 and 1.2 mol% Gd<sub>2</sub>O<sub>3</sub>, the resistivities of grain boundaries are determined as 52.9, 24.5 and 21.2 MΩ · cm at the frequency of 40 Hz, respectively. One can see that doping Gd<sub>2</sub>O<sub>3</sub> causes the boundary resistivities to decrease and the grain resistivities to increase. Table 1 shows the characteristic detail of the varistor system.

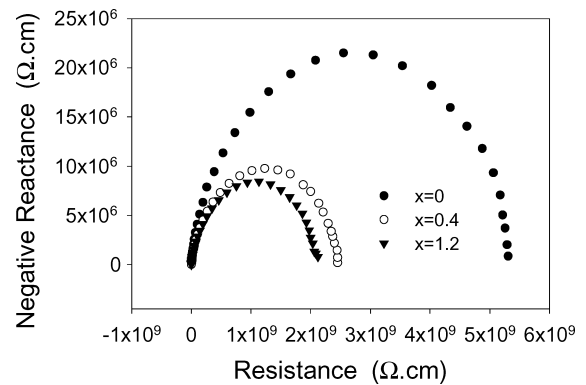
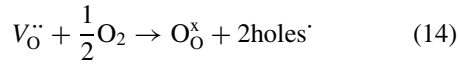


Fig. 5. Impedance diagrams for (99.15 -  $x$ )%SnO<sub>2</sub> + 0.75%Co<sub>2</sub>O<sub>3</sub> + 0.1%Ta<sub>2</sub>O<sub>5</sub> +  $x$ % Gd<sub>2</sub>O<sub>3</sub>.

Due to the lattice distortion caused by the substitution of Sn<sup>4+</sup> with Gd<sup>3+</sup>, the oxygen vacancy V<sub>O</sub><sup>••</sup> in Eq. (11) is energetically unfavorable and may easier react with gaseous oxygen according to the equation



The recombination between the holes of Eq. (14) and the electrons in SnO<sub>2</sub> grains will result in the decrease in electrons concentration of SnO<sub>2</sub> grains. That may be the reason why the grain resistivity of the SnO<sub>2</sub>-based varistors increased with increasing Gd<sub>2</sub>O<sub>3</sub> concentration.

### Conclusions

- (1) Gd<sub>2</sub>O<sub>3</sub> addition has a great effect on electrical properties of the (Co, Nb)-doped SnO<sub>2</sub>. Gd<sub>2</sub>O<sub>3</sub> can substantially raise the threshold voltage (Co, Ta)-doped SnO<sub>2</sub> and lower the permittivity of the (Co, Ta)-doped SnO<sub>2</sub>. The significant decrease of the SnO<sub>2</sub> grain size, from 3.8 to 1.6 μm with increasing Gd<sub>2</sub>O<sub>3</sub> concentration over the range of 0 to 1.2 mol%, is the origin for raising the threshold voltage and lowering the dielectric constants.
- (2) Because the ionic radius of Gd<sup>3+</sup> is larger than that of Sn<sup>4+</sup>, the process of the substitution of Sn<sup>4+</sup> by Gd<sup>3+</sup> is relatively difficult to occur. Gd<sub>2</sub>O<sub>3</sub> residing at SnO<sub>2</sub> grain boundaries may hinders the SnO<sub>2</sub> grains on its both sides from conglomerating into large particles. That may be the reason why the mean grain size of the SnO<sub>2</sub> based varistors decreased significantly with increasing Gd<sub>2</sub>O<sub>3</sub> concentration.
- (3) The SnO<sub>2</sub> varistors doped with 0.8 and 1.2 mol% Gd<sub>2</sub>O<sub>3</sub> have superhigh threshold voltage and larger

nonlinear coefficient  $\alpha$ . Superhigh threshold voltage and quite larger nonlinear coefficient  $\alpha$  qualify the Gd-doped SnO<sub>2</sub> varistor as an excellent candidate in use for the high voltage protection system.

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